

# UTILITY PATENT APPLICATION TRANSMITTAL

Attorney Docket No. 1004.1063/JDH

First Named Inventor or Application Identifier:

Toshihiko MIURA, et al.

Express Mail Label No.

(Only for new nonprovisional applications under 37 CFR 1.53(b))

 JC675 U.S. PTO  
09/419798


16/18/99

## APPLICATION ELEMENTS

See MPEP chapter 600 concerning utility patent application contents.

 ADDRESS TO: Assistant Commissioner for Patents  
Box Patent Application  
Washington, DC 20231

1. ☒ Fee Transmittal Form
2. ☒ Specification, Claims & Abstract ..... [ Total Pages: 16 ]
3. ☒ Drawing(s) (35 USC 113) ..... [ Total Sheets: 8 ]
4. ☒ Oath or Declaration ..... [ Total Pages: 1 ]
  - a. ☒ Newly executed (original or copy)
  - b. ☐ Copy from a prior application (37 CFR 1.63(d)) (for continuation/divisional with Box 17 completed)
    - i. ☐ DELETION OF INVENTOR(S)  
Signed statement attached deleting inventor(s) named in the prior application, see 37 CFR 1.63(d)(2) and 1.33(b).
5. ☐ Incorporation by Reference (usable if Box 4b is checked)  
The entire disclosure of the prior application, from which a copy of the oath or declaration is supplied under Box 4b, is considered as being part of the disclosure of the accompanying application and is hereby incorporated by reference therein.
6. ☐ Microfiche Computer Program (Appendix)
7. ☐ Nucleotide and/or Amino Acid Sequence Submission (if applicable, all necessary)
  - a. ☐ Computer Readable Copy
  - b. ☐ Paper Copy (identical to computer copy)
  - c. ☐ Statement verifying identity of above copies

## ACCOMPANYING APPLICATION PARTS

8. ☒ Assignment Papers (cover sheet & document(s))
9. ☐ 37 CFR 3.73(b) Statement (when there is an assignee) [ ] Power of Attorney
10. ☐ English Translation Document (if applicable)
11. ☐ Information Disclosure Statement (IDS)/PTO-1449 [ ] Copies of IDS Citations
12. ☒ Preliminary Amendment
13. ☒ Return Receipt Postcard (MPEP 503) (Should be specifically itemized)
14. ☐ Small Entity Statement(s) [ ] Statement filed in prior application, status still proper and desired.
15. ☐ Certified Copy of Priority Document(s) (if foreign priority is claimed)
16. ☐ Other:

17. If a CONTINUING APPLICATION, check appropriate box and supply the requisite information:

[ ] Continuation [ ] Divisional [ ] Continuation-in-part (CIP) of prior application No:      /     

## 18. CORRESPONDENCE ADDRESS

 STAAS & HALSEY  
Attn: James D. Halsey, Jr.  
700 Eleventh Street, N.W., Suite 500  
Washington, DC 20001

 Telephone: (202) 434-1500  
Facsimile: (202) 434-1501

 jc639 U.S. PTO  
10/18/99

09449798 "101899"

**NEW APPLICATION  
FEE TRANSMITTAL**

Attorney Docket No. 1004.1063/JDH  
 Application Number Unassigned  
 Filing Date October 18, 1999

AMOUNT ENCLOSED \$ 800.00 First Named Inventor Toshihiko MIURA, et al.

**FEE CALCULATION** (fees effective 10/01/97)

CLAIMS	(1) FOR	(2) NUMBER FILED	(3) NUMBER EXTRA	(4) RATE	(5) CALCULATIONS
TOTAL CLAIMS	2	- 20 =	0	X \$ 18.00 =	\$ 0.00
INDEPENDENT CLAIMS	1	- 3 =	0	X \$ 78.00 =	0.00
MULTIPLE DEPENDENT CLAIMS (any number; if applicable)				+ \$270.00 =	0.00
				<b>BASIC FILING FEE</b>	+ 760.00
				Total of above Calculations =	\$ 760.00
Surcharge for late filing fee, Statement or Power of Attorney (\$130.00)					+ 0.00
Reduction by 50% for filing by small entity (37 CFR 1.9, 1.27 & 1.28).					- 0.00
				<b>TOTAL FILING FEE =</b>	\$ 760.00
Surcharge for filing non-English language application (\$130.00; 37 CFR 1.52(d))					+ 0.00
Recordation of Assignment (\$40.00; 37 CFR 1.21(h)(1))					40.00
				<b>TOTAL FEES DUE =</b>	\$ 800.00

**METHOD OF PAYMENT**

- ☒ Check enclosed as payment.  
☐ Charge "TOTAL FEES DUE" to the Deposit Account No., below.  
☐ No payment is enclosed and no charges to the Deposit Account are authorized at this time.

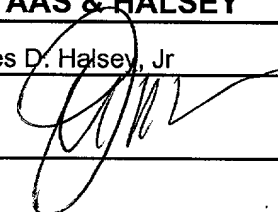
**GENERAL AUTHORIZATION**

- ☒ If the above-noted "AMOUNT ENCLOSED" is not correct, the Commissioner is hereby authorized to credit any overpayment or charge any additional fees necessary to:

Deposit Account No. 19-3935  
 Deposit Account Name STAAS & HALSEY

- ☒ The Commissioner is also authorized to credit any overpayments or charge any additional fees required under 37 CFR 1.16 (filing fees) or 37 CFR 1.17 (processing fees) during the prosecution of this application, including any related application(s) claiming benefit hereof pursuant to 35 USC § 120 (e.g., continuations/divisionals/CIPs under 37 CFR 1.53(b) and/or continuations/divisionals/CPAs under 37 CFR 1.53(b)) to maintain pendency hereof or of any such related application.

**SUBMITTED BY: STAAS & HALSEY**

Typed Name	James D. Halsey, Jr	Reg. No.	22,729
Signature		Date	October 18, 1999

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re Application of:

Toshihiko MIURA, et al.

Serial No.: To Be Assigned

Group Art Unit: To Be Assigned

Filed: October 18, 1999

Examiner: To Be Assigned

For: RESIN BONDED RARE EARTH MAGNET

**PRELIMINARY AMENDMENT**

Assistant Commissioner of Patents  
Washington, D.C. 20231

Sir:

Before examination of the above-identified application, please amend the application as follows:

**IN THE SPECIFICATION:**

Please AMEND the specification as follows:

Page 3, line 1, change "not possible" to --impossible--;

line 6, delete "thick film" and after "magnet" insert --coated by a thick film--.

Page 4, line 13, delete "and harden".

Page 5, line 18, delete "Sm-Fe-N or Sm-Co, etc."; and before "made" insert --or--;

line 19, after "HDDR)" insert --Sm-Fe-N or Sm-Co, etc.--.

Page 7, line 25, delete "at room temperature"; and after "resin" insert --at room temperature--.

Page 11, line 25, change "(BHmax)" to --(BH) max--.

Page 12, line 8, change "Into" to --When--.

Page 16, line 8, after "Claim 2" insert a new page.

**IN THE ABSTRACT:**

Line 4, delete "body".

**REMARKS**

This Preliminary Amendment is submitted to improve the form of the claims as originally-filed.

It is respectfully requested that this Preliminary Amendment be entered in the above-referenced application.

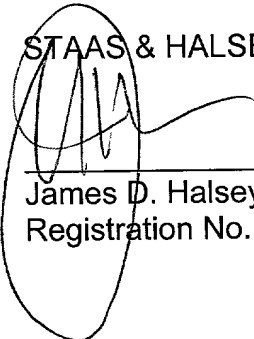
If any further fees are required in connection with the filing of this Preliminary Amendment, please charge same to our Deposit Account No. 19-3935.

Respectfully submitted,

STAAS & HALSEY

Date: October 18, 1999

By:

  
James D. Halsey, Jr.  
Registration No. 22,729

700 Eleventh Street, N.W., Suite 500  
Washington, D.C. 20001  
(202) 434-1500

## TITLE OF THE INVENTION

Resin bonded rare earth magnet

## BACKGROUND OF THE INVENTION

### 1. Field of the Invention

The present invention provides a resin bonded rare earth magnet with superior corrosion resistance due to suppression of roughness on the surface of the magnet.

### 2. Description of the Prior Art

Rare earth magnets made from rare earth metals and transition metals have found widespread use in recent years due to the remarkable superiority of their magnetic characteristics compared to ferrite or Alnico magnets. However, because Nd-Fe-B rare earth magnets easily oxidize under the condition of high temperature and high humidity, resulting in the formation of rust and degradation of magnetic characteristics, resin or metallic coatings have been applied to the magnet surface to inhibit oxidation. Especially for bonded magnets made from Nd-Fe-B quenched powder and organic resin, it has been customary to use spraying or electrolytic deposition to apply a resin coating or nickel plating to the surface of the molded body.

In rare earth bonded magnets, which are mainly used in PM stepping motors or the spindle motors for CD-ROM drives, high quality is required for magnetic characteristics and corrosion resistance in order to achieve more compact size and

lower power consumption. Especially, as the storage density of hard disk drives increases, this is accompanied by requirements for cleaner and faster spindle motors, and accordingly it has become important that the magnets mounted in such motors have sufficient corrosion resistance and strength, and are free from adhering organic particles, etc.

Conventionally, the surface of bonded magnets is coated with epoxy or acrylic resin to improve corrosion resistance. However, because magnetic particles of irregular sizes ranging from a few tens to a few hundreds of microns in diameter are fixed in a small quantity of resin bond, there will be a large number of protrusions or depressions in the surface of the magnet. Because of this, the thickness of the coating will not be even and the smoothness of the surface cannot be ensured. Defects such as pinholes and air bubbles easily occur, which will lead to deterioration of the corrosion resistance. Moreover, since the coating may not fully cover some projecting magnetic particles which are exposed at the magnet surface, such particles may break off during the rotation of a spindle motor and cause interference with the rotation.

To overcome this problem, attempts have been made to use magnetic particles having a particle size of 10 microns or less to minimize roughness on the magnet surface. However in this case the magnetic density produced by compression molding is insufficient and the desired magnetic characteristics cannot be

obtained. It is also not possible to greatly reduce the roughness on the surface of the magnet by improving the methods of forming the coating using coating or electrolytic deposition. Accordingly, a thick film coating with a thickness of several tens of microns must be employed in order to achieve sufficient corrosion resistance. However, if such a thick film magnet is used in a spindle motor, because of the thickness of the coating, the effective magnetic flux per volume of the magnet will be reduced, which is inconvenient for the motor characteristics. In these circumstances, there is a requirement for a powerful resin bonded rare earth magnet with good corrosion resistance, in which the roughness of the magnet surface has been suppressed.

In view of the conditions described above, the present invention has the objective of providing a resin bonded rare earth magnet, compression molded from rare earth-transition metal powder and thermosetting resin, in which a corrosion inhibiting coating made from synthetic resin which covers the surface of the compression molded magnet is made as thin as possible while preventing the occurrence of defects such as air bubbles and pinholes.

#### SUMMARY OF THE INVENTION

In order to achieve the above-mentioned objective, the main present invention provides a resin bonded rare earth magnet, compression molded from rare earth-transition metal

09413798-10159  
658707-86267450

powder and thermosetting resin, having a magnet comprising a mixture of thermosetting resin and rare earth-transition metal powder with a particle size of between 20 and 300 microns, a filling material with particle size between 0.1 and 15 microns which is used to fill in the depressions in the surface of said magnet body and is then fixed with resin, and a corrosion inhibiting coat made from synthetic resin applied to the surface of said magnet which has been rendered smooth by the application of said filling material into the depressions in its surface.

The second present invention provides a resin bonded rare earth magnet according to the above mentioned main present invention, having the characteristic that said filling material, used to fill and harden the depressions on the surface of said magnet, employs a thermosetting resin to fixed the filling material in the depressions.

The third present invention provides a resin bonded rare earth magnet according to main present invention, having the characteristic that the corrosion inhibiting coat made from synthetic resin applied to the surface of said magnet has a thickness of between 1 and 30 microns.

#### BRIEF DESCRIPTION OF THE DRAWINGS

FIG 1 is a cross sectional view of a resin bonded rare earth magnet as related by the present invention.

FIG 2 is a perspective view showing the roughness on the



surface of the magnet body.

FIG 3 is a perspective view showing the said roughness on the surface of the magnet having been filled with filling material.

FIG 4 is a table showing the relationship between surface roughness and the occurrence of corrosion.

FIG 5 is a table giving the results of example of execution 1.

FIG 6 is a table giving the results of example of execution 2.

FIG 7 is a table giving the results of example of execution 3.

#### DETAIL DESCRIPTION OF THE INVENTION

The following explanation will describe how the present invention achieves a resin bonded rare earth magnet with a remarkably small amount of roughness on the magnet surface. The rare earth alloy used in the present invention employs rare earth transition metal powder such as Nd-Fe-B made using the melt quenching method, Sm-Fe-N or Sm-Co, etc. made using hydrogen adsorption (by the method known as HDDR). A particle size between several microns and several hundreds of microns may be used, but the present invention requires a size of 20 to 300 microns. With particles smaller than 20 microns, the required density cannot be obtained without very greatly increasing the forming pressure employed in the compression molding process

and accordingly the desired magnetic characteristics are hard to obtain and mold breakages are common. With particles over 300 microns in size, the roughness of the magnet surface becomes very great, the roughness are extremely difficult to smooth away and the external appearance is degraded.

Solid or liquid resin such as epoxy, phenol, melamine, etc. may be used as the thermosetting resin to be mixed with the above described magnetic powder, and, using the compression molding method, the ratio of the mixture is normally within the range 1 to 5% by weight of resin to magnetic powder. Other additives used may include silane coupling agent to improve the coupling between metal and resin, and fatty acids or their salts in order to improve the lubrication during forming. Normally available equipment may be used to process the magnetic powder, resin and additives by mixing, stirring, powdering and other processes, and shaping the body by filling in a metal mold to obtain the magnet illustrated in FIG 1. Further, by selection of alloy powder and forming in a magnetic field, an anisotropic magnet body can be obtained.

Several methods, as described below, may be employed to achieve a smooth molded magnet body with little surface roughness. Increasing the ratio of resin to magnetic powder will reduce air holes in the molded body surface. By adding lubricating additives such as fatty acids, or by coating the mold with a lubricating agent such as boron nitride, friction at the

molded body surface may be reduced. And using a high density filling of magnetic powder reduces air holes in and around the molded body.

Further, as shown in FIG 1, by filling the depressions 2 in the surface of magnet body 1 with inorganic filler material 3, roughness on the surface can be reduced to obtain a smooth, level surface. Examples of inorganic filler materials that may be used are oxides such as  $\text{Al}_2\text{O}_3$ ,  $\text{SiO}_2$  and  $\text{TiO}_2$ , various kinds of carbides, borides, nitrides and sulfides, and also graphite and other corrosion resistant metal or alloy powders. In order to fill the spaces between the magnetic particles, the particle size of the filler must be within the range 0.1 to 15 microns in order to achieve the objective of a surface roughness  $R_a$  of 3 microns or less. If the size is less than 0.1 micron, there will be a tendency for the filler to accumulate on the level surfaces as well as in the spaces between particles, and thus the effect will be the reverse of that intended and the surface will actually become rougher. Small particles will also float off easily into the air, making handling more difficult. On the other hand, filler particles over 15 microns in size will fill in only the larger of the spaces between magnetic particles and leave smaller spaces empty, thus the objective of a surface roughness  $R_a$  of 3 or less microns will not be achieved.

As an example of a filling method to be used for inorganic filling material 3,  $\text{TiO}_2$  powder of 1.5 micron particle size is mixed with at room temperature powdered epoxy resin in a 1: 1

ratio. This mixture is placed, together with the molded magnet body and alumina balls in a pot, where ball milling occurs for 10 minutes. Next, the molded magnet body, the surface of which has been filled by the  $\text{TiO}_2$  and epoxy powder filler, is shaken on a vibrating sieve to remove the excess filling agent. Epoxy curing is then performed by heating at 120 to 150 ° C for 30 minutes, which fixes the  $\text{TiO}_2$  on the surface of the molded body. Other possible methods include the use of liquid thermosetting resin and the use of other types of mixing machines to replace ball milling. FIGS 2 and 3 show the surface of the molded magnet body before and after filling with powders  $\text{TiO}_2$ . It can be seen that the result of this process is to greatly reduce irregularities and air holes in the surface of the sample. The surface roughness of this sample before filling was 4.1 microns, and after filling the Ra was 1.8 microns.

In the case of resin bonded rare earth magnets, a corrosion inhibiting coat 4 of thickness between 1 and 30 microns is normally applied to the surface of magnet body 1 using spray coating, electrolytic deposition, nickel plating etc., for the purpose of improving the corrosion resistance of said surface and for preventing magnetic particles coming free from said surface. In this case, the surface roughness after the corrosion inhibiting coat is applied depends on the surface roughness of the molded body, and if the surface of magnet body 1 is smooth and level, then necessarily the surface after application of the corrosion

inhibiting coat will also be smooth and level, the roughness value Ra being approximately the same before and after applying said coat. Furthermore, high temperature and high humidity test results show that the corrosion resistance will become greater as the surface roughness after application of the corrosion inhibiting coat becomes smaller, and accordingly it can be seen that as the surface roughness becomes smaller, the coating required can be made thinner.

To achieve the objective of the present invention of providing a highly corrosion resistant magnet, it is necessary that the surface roughness Ra of the magnet surface be less than 3 microns after the corrosion inhibiting coat has been applied. If the roughness exceeds 3 microns, the depressions and projections on the magnet will be too large to be smoothed out by the application of filling agent and the corrosion inhibiting coat, and so corrosion resistance cannot be assured.

FIG 4 shows the relationship between surface roughness Ra of an Nd-Fe-B type bonded magnet and the occurrence of corrosion. Magnet samples of different roughnesses were prepared by varying the amount of TiO<sub>2</sub> and powdered epoxy filling applied to the surface of a cylindrical molded body having a diameter of 12 mm and a length of 10 mm, a 20 micron thick epoxy coating then being sprayed onto this. The surface roughness was then measured using a surface roughness tester. Corrosion resistance was evaluated by the amount of corrosion

present after 500 hours exposure to high temperature and high humidity (70° C and 95% RH). (Symbols used in FIG 4: ○; no change, △; some swelling, ×; red rust present)

As can be seen from FIG 4, the amount of surface roughness affects the corrosion resistance of the magnet samples, with the desired corrosion resistance being assured when Ra is 2 microns or less. Furthermore, when a magnet with small surface roughness is given a uniform coating over the entire magnet surface, this will eliminate the danger of particles breaking loose during the work of mounting the magnet or assembling the motor, thus making it ideal for hard disk drive motors which require especially clean operating environments. Below, the present invention will be described in greater detail through various examples of execution.

#### Example of Execution 1

Quenched flakes of Nd-Fe-B are pulverized to obtain powder with particle sizes of 10 or less, 20 to 45, 45 to 105, 45 to 180, 45 to 300 and 45 to 500 microns. These powders are mixed, stirred and granulated 1.5 to 3.0% by weight of liquid epoxy resin as bonding material, and 0.2% by weight of oleic acid as lubricating agent. Next the granulated powder is compression molded at 1GPa in a metal mold, and the resin is cured by heating for 1 hour at 150° C to obtain a molded magnet with the dimensions of external diameter 18 mm, internal diameter 16 mm and length 3 mm. Next, 1.5 micron TiO<sub>2</sub> powder is mixed with

epoxy resin powder in the ratio 1:1 by mass, and this mixture is placed, together with the molded magnet and alumina balls, in a pot, where ball milling is performed for 10 minutes. Next, the molded magnet is shaken on a vibrating sieve to remove the excess  $\text{TiO}_2$  and epoxy powder filler, and curing is then performed by heating at  $150^\circ \text{C}$  for 30 minutes. Finally, after cleaning with purified water, an epoxy coating is sprayed on to give the magnet sample a corrosion resistant coat 20 microns in thickness. The surface roughness of the sample is measured by a surface roughness tester, and the magnetic characteristics are measured using a BH tracer. A corrosion resistance test evaluated the amount of corrosion present on the sample after 500 hours exposure to high temperature and high humidity ( $70^\circ \text{C}$  and 95% RH). The results of the test are shown in FIG 5.

FIG 5 shows how magnet surface roughness increases with an increase in magnetic powder particle size. Sample (f), with a particle size of 45 to 500 microns, gives an  $R_a$  of 3.9 microns, and after the corrosion resistance test, swellings could be observed on the surface. Underneath these swellings in the coating, it was found that red rust had occurred. On the other hand, with sample (a) of particle size 10 microns or less, surface roughness was slight and no evidence of rusting was found. However, since the particle size was too small, good forming density was not achieved and so the desired magnetic characteristics ( $\text{BH}_{\text{max}}$ ) were not obtained. Samples (b) to (e),

with the magnetic powder particle size specified by the present invention of between 20 and 300 microns, achieved the desired magnetic characteristics and also satisfied the requirement for corrosion resistance.

(Symbols used in FIG 5: ○; no change, △; some swelling)

#### Example of Execution 2

Quenched flakes of Nd-Fe-B are pulverized to obtain powder with particle sizes of 45 to 180 microns. Into these powder are mixed, stirred and granulated 2.0% by weight of liquid epoxy resin as bonding material, and this granulated powder is compression molded in the same way as Example of Execution 1, and the resin is cured by heating for 1 hour at 150° C to obtain a molded magnet with the dimensions of external diameter 18 mm, internal diameter 16 mm and length 3 mm. Next, 0.05 to 20 micron SiO<sub>2</sub> powder is mixed with epoxy resin powder in the ratio 2:1 by mass, and this mixture is placed, together with the molded magnet and alumina chips, into a planetary rotating pot, and rotated for 10 minutes. Next, the excess powder is removed, and curing is performed by heating at 150 ° C for 30 minutes. Finally, after cleaning with purified water, a 15 micron thick epoxy coating is sprayed on and cured. The same corrosion resistance test as Example of Execution 1 was performed, the results of which are shown in FIG 6.

FIG 6 shows how magnet surface roughness depends on the particle size of the SiO<sub>2</sub> used as filler, and shows how this



also affects the occurrence of rust. In sample (g), the SiO<sub>2</sub> particle size is too small, the spaces between magnet particles are not filled sufficiently and particles of filler accumulated on the surface so no improvement in surface roughness was achieved. On the other hand, in sample (m) the SiO<sub>2</sub> particle size is too large and only some of the spaces were filled. Samples (h) to (l), with the filling agent particle size specified by the present invention of between 0.1 and 15 microns, achieved the desired magnetic characteristics with no rust being generated.

(Symbols used in FIG 6: ○; no change, △; some swelling, ×; red rust present)

#### Example of Execution 3

Anisotropic Nd-Fe-B powder having an average particle size of 120 microns was mixed with 2.0% by weight of liquid epoxy resin and 0.2% by weight of stearic acid and stirred and granulated. Next, the granules were compression molded in a magnetic field of 800 kA/m at a pressure of 0.6 to 1.6 GPa and the resin cured by heating for 1 hour at 150° C to obtain a molded magnet body with the dimensions of external diameter 12 mm and length 10 mm. In this case, the metal mold used has an interior surface roughness of the die of 0.6 microns, greater than the 0.1 micron of a normal lap grinder surface. The reason for this is to increase the friction of the molded body surface during the powder compression process and make it easy to remove excess magnetic powder positioned on the surface layer, the result being

to make the surface roughness of the molded body smaller. The molded body was given an epoxy coating 15 microns thick, and this was used as the test sample. Test sample density and magnetic characteristics were measured, and the same corrosion resistance test as for Example of Execution 1 was performed, the results of which are shown in FIG 7.

From FIG 7, it can be seen that increasing the molding pressure improves the magnet density and the magnetic characteristics, surface roughness becomes smaller and rusting is suppressed. In test samples (n) and (o), the magnet density is not sufficient, so large spaces exist in the surface and surface roughness remains larger. These results show that samples (p) to (s) having surface roughness of 3 microns or less, as specified by the present invention, had good corrosion resistance.

(Symbols used in FIG 7: ○; no change, △; some swelling, ×; red rust present)

The present invention has been described in connection with the above-mentioned embodiments, but it will be understood that various changes and applications can be made therein within the true spirit of the present invention, and these changes and applications are not excluded from the scope of the present invention.

In described above, the present invention provides a means for providing a clean, high performance magnet suitable for use in the drive motors of hard disk drives and CD-ROM drives,

in which the depressions occurring in the surface of the magnet are filled by a filling agent having a particle size smaller than that of the depressions, thus substantially making the surface of the magnet level and reducing the surface roughness Ra to 3 microns or less, and, when a corrosion inhibiting coat of synthetic resin is applied to the surface, the surface of said corrosion inhibiting coat is made substantially smooth thus providing a surface roughness the same as that of the magnet, the effect of forming such an extremely level corrosion inhibiting coat being that the coat can be applied as thinly as 1 to 30 microns in thickness without defects such as pinholes or bubbles occurring, and the magnet has superior corrosion resistance as well as no danger of magnetic particles coming loose from the surface.

What we claimed is:

1, A resin bonded rare earth magnet, compression molded from rare earth-transition metal alloy powder and thermosetting resin, comprising:

a magnet body comprising a mixture of thermosetting resin and rare earth-transition metal alloy powder with a particle size of between 20 and 300 microns;

a filling material with particle size between 0.1 and 15 microns which is used to fill in the depressions on the surface of said magnet and is then fixed with said thermosetting resin; and

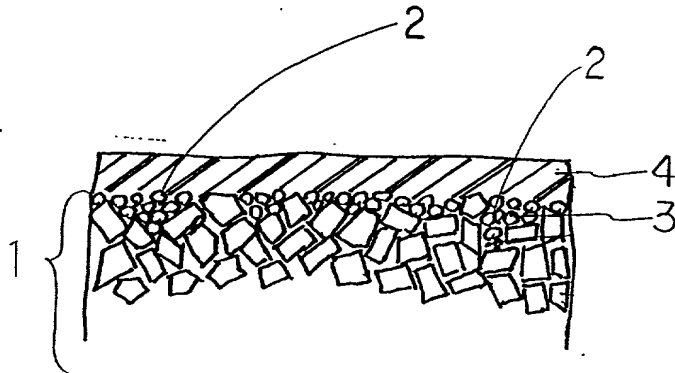
a corrosion inhibiting coat made from synthetic resin applied to the surface of said magnet which has been rendered smooth by the application of said filling material into the depressions on its surface.

2, A resin bonded rare earth magnet according to Claim 1, wherein the corrosion inhibiting coat made from synthetic resin applied to the surface of said magnet has a thickness of between 1 and 30 microns.

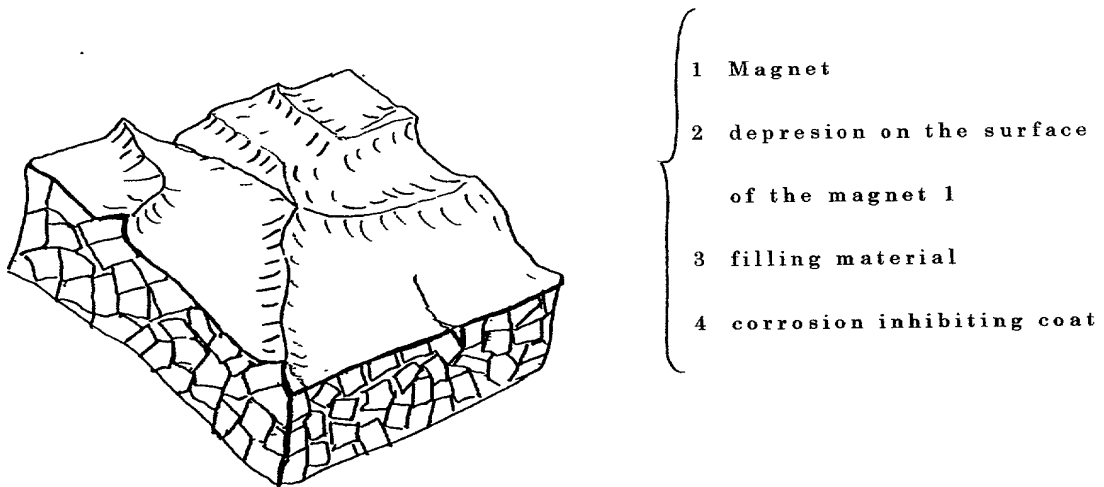
#### ABSTRACT

A resin bonded rare earth magnet, compression molded from rare earth-transition alloy powder and thermosetting resin, having a magnet body 1 comprising a mixture of thermosetting resin and rare earth-transition alloy powder with a particle size of between 20 and 300 microns, a filling material 3 with particle size between 0.1 and 15 microns which is used to fill in the depressions 2 on the surface of said magnet 1 and is then fixed with said thermosetting resin, and a corrosion inhibiting coat 4 made from synthetic resin applied to the surface of said magnet 1 which has been rendered smooth by the application of said filling material into the depressions on its surface.

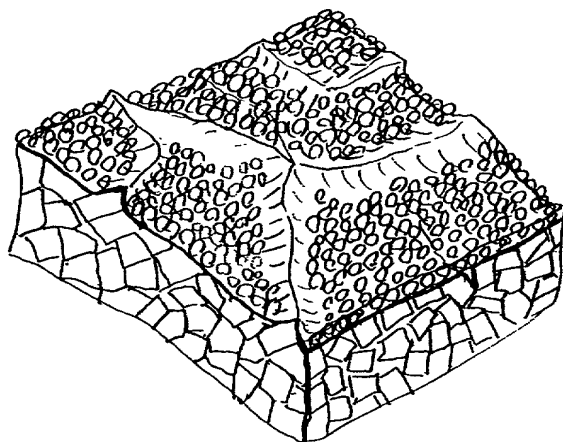
【 Fig.1】



【 Fig.2】



【 Fig.3】



【 Fig.4】

ROUGHNESS Ra ( $\mu$ m )	1.2	1.8	2.3	2.7	3.6	4.4
THE AMOUNT OF CORROSION PRESENT	○	○	○	○	△	×

\* (SYMBOLS USED IN THE ABOVE CHART:

○ : NO CHANGE, △ : SOME SWELLING, × : RED RUSH PRESENT)

Figure 1 consists of 12 sub-graphs, labeled (a) through (l), each showing a time course of a different physiological parameter. The x-axis for all graphs represents time, with a baseline period followed by a 10-minute intervention period. The y-axis for each graph represents the value of the parameter. The parameters are: (a) Heart rate (b/min), (b) Systolic blood pressure (mmHg), (c) Diastolic blood pressure (mmHg), (d) Mean arterial pressure (mmHg), (e) Cardiac output (l/min), (f) Stroke volume (ml), (g) Stroke volume index (ml/m²), (h) Stroke volume index (ml/m²), (i) Stroke volume index (ml/m²), (j) Stroke volume index (ml/m²), (k) Stroke volume index (ml/m²), and (l) Stroke volume index (ml/m²). The graphs show that during the 10-minute intervention, heart rate, systolic blood pressure, diastolic blood pressure, mean arterial pressure, cardiac output, stroke volume, and stroke volume index all decrease or stabilize at a lower level compared to the baseline.

Figure 1 consists of 12 sub-graphs labeled (a) through (l), each plotting a different physiological parameter against time (0 to 10 minutes). The graphs compare three conditions: Control (solid line), 10 min (dashed line), and 20 min (dotted line). The parameters and their approximate y-axis scales are: (a) HR (b/min) 0-180, (b) SV (ml) 0-100, (c) CO (l/min) 0-10, (d) MAP (mmHg) 0-100, (e) PVR (mmHg) 0-10, (f) SVR (mmHg) 0-10, (g) PPA (mmHg) 0-10, (h) PVP (mmHg) 0-10, (i) PVP/PPA 0-10, (j) PVP/PPA 0-10, (k) PVP/PPA 0-10, and (l) PVP/PPA 0-10. The graphs show various trends, such as increases or decreases in heart rate, stroke volume, and blood pressure over time for each condition.

Figure 1 consists of 12 sub-graphs labeled (a) through (l), each plotting a different physiological parameter against time (0 to 10 minutes). The graphs compare three conditions: Control (solid line), 10 min (dashed line), and 20 min (dotted line). The parameters and their approximate y-axis scales are: (a) HR (b/min) 0-180, (b) SV (ml) 0-100, (c) CO (l/min) 0-10, (d) MAP (mmHg) 0-100, (e) PVR (mmHg) 0-10, (f) SVR (mmHg) 0-10, (g) PPA (mmHg) 0-10, (h) PVP (mmHg) 0-10, (i) PVP/PPA 0-10, (j) PVP/PPA 0-10, (k) PVP/PPA 0-10, and (l) PVP/PPA 0-10. The graphs show various trends, such as increases or decreases in heart rate, stroke volume, and blood pressure over time for each condition.

Figure 1 consists of 12 sub-graphs labeled (a) through (l), each plotting a different physiological parameter against time (0 to 10 minutes). The graphs compare three conditions: Control (solid line), 10 min (dashed line), and 20 min (dotted line). The parameters and their approximate y-axis scales are: (a) HR (b/min) 0-180, (b) SV (ml) 0-100, (c) CO (l/min) 0-10, (d) MAP (mmHg) 0-100, (e) PVR (mmHg) 0-10, (f) SVR (mmHg) 0-10, (g) PPA (mmHg) 0-10, (h) PVP (mmHg) 0-10, (i) PVP/PPA 0-10, (j) PVP/PPA 0-10, (k) PVP/PPA 0-10, and (l) PVP/PPA 0-10. The graphs show various trends, such as increases or decreases in heart rate, stroke volume, and blood pressure over time for each condition.

Figure 1 consists of 12 sub-graphs labeled (a) through (l), each plotting a different physiological parameter against time (0 to 10 minutes). The graphs compare three conditions: Control (solid line), 10 min (dashed line), and 20 min (dotted line). The parameters and their approximate y-axis scales are: (a) HR (b/min) 0-180, (b) SV (ml) 0-100, (c) CO (l/min) 0-10, (d) MAP (mmHg) 0-100, (e) PVR (mmHg) 0-10, (f) SVR (mmHg) 0-10, (g) PPA (mmHg) 0-10, (h) PVP (mmHg) 0-10, (i) PVP/PPA 0-10, (j) PVP/PPA 0-10, (k) PVP/PPA 0-10, and (l) PVP/PPA 0-10. The graphs show various trends, such as increases or decreases in heart rate, stroke volume, and blood pressure over time for each condition.

Figure 1 consists of 12 sub-graphs labeled (a) through (l), each plotting a different physiological parameter against time (0 to 10 minutes). The graphs compare three conditions: Control (solid line), 10 min (dashed line), and 20 min (dotted line). The parameters and their approximate y-axis scales are: (a) HR (b/min) 0-180, (b) SV (ml) 0-100, (c) CO (l/min) 0-10, (d) MAP (mmHg) 0-100, (e) PVR (mmHg) 0-10, (f) SVR (mmHg) 0-10, (g) PPA (mmHg) 0-10, (h) PVP (mmHg) 0-10, (i) PVP/PPA 0-10, (j) PVP/PPA 0-10, (k) PVP/PPA 0-10, and (l) PVP/PPA 0-10. The graphs show various trends, such as increases or decreases in heart rate, stroke volume, and blood pressure over time for each condition.

Figure 1 consists of 12 sub-graphs labeled (a) through (l), each plotting a different physiological parameter against time (0 to 10 minutes). The graphs compare three conditions: Control (solid line), 10 min (dashed line), and 20 min (dotted line). The parameters and their approximate y-axis scales are: (a) HR (b/min) 0-180, (b) SV (ml) 0-100, (c) CO (l/min) 0-10, (d) MAP (mmHg) 0-100, (e) PVR (mmHg) 0-10, (f) SVR (mmHg) 0-10, (g) PPA (mmHg) 0-10, (h) PVP (mmHg) 0-10, (i) PVP/PPA 0-10, (j) PVP/PPA 0-10, (k) PVP/PPA 0-10, and (l) PVP/PPA 0-10. The graphs show various trends, such as increases or decreases in heart rate, stroke volume, and blood pressure over time for each condition.

Figure 1 consists of 12 sub-graphs labeled (a) through (l), each plotting a different physiological parameter against time (0 to 10 minutes). The graphs compare three conditions: Control (solid line), 10 min (dashed line), and 20 min (dotted line). The parameters and their approximate y-axis scales are: (a) HR (b/min) 0-180, (b) SV (ml) 0-100, (c) CO (l/min) 0-10, (d) MAP (mmHg) 0-100, (e) PVR (mmHg) 0-10, (f) SVR (mmHg) 0-10, (g) PPA (mmHg) 0-10, (h) PVP (mmHg) 0-10, (i) PVP/PPA 0-10, (j) PVP/PPA 0-10, (k) PVP/PPA 0-10, and (l) PVP/PPA 0-10. The graphs show various trends, such as increases or decreases in heart rate, stroke volume, and blood pressure over time for each condition.

【 Fig.7】

SAMPLE NAMES	MOLDING PRESSURE (GPa)	MAGNET DENSITY ( $\times 10^3 \text{ kg/m}^3$ )	BH <sub>max</sub> ( $\text{kJ/m}^3$ )	SURFACE ROUGHNESS Ra ( $\mu \text{ m}$ )	OCCURRENCE OF CORROSION*
SAMPLE (n)	0.6	5.84	103	4.1	×
SAMPLE (o)	0.8	6.04	118	3.3	△
SAMPLE (p)	1.0	6.17	132	2.2	○
SAMPLE (q)	1.2	6.28	141	1.6	○
SAMPLE (r)	1.4	6.36	149	1.4	○
SAMPLE (s)	1.6	6.43	154	1.3	○

\* (SYMBOLS USED IN THE ABOVE CHART:

○ : NO CHANGE, △ : SOME SWELLING, × : RED RUSH PRESENT)



## COMBINED DECLARATION/POWER OF ATTORNEY FOR UTILITY/DESIGN PATENT APPLICATION

Full name of third joint inventor, if any Shunji SuzukiInventor's Signature Shunji Suzuki Date October 5, 1999Residence Same as below Citizenship JapanesePost Office Address c/o Minebea Co., Ltd. R&D Center  
1743-1 Asana, Asaba-cho, Iwata-gun, Shizuoka-ken, JapanFull name fourth joint, inventor, if any Shuichi NishidaInventor's Signature Shuichi Nishida Date October 5, 1999Residence Same as below Citizenship JapanesePost Office Address c/o Minebea Co., Ltd. R&D Center  
1743-1 Asana, Asaba-cho, Iwata-gun, Shizuoka-ken, Japan

Full name of fifth joint inventor, if any \_\_\_\_\_

Inventor's Signature \_\_\_\_\_ Date \_\_\_\_\_

Residence \_\_\_\_\_ Citizenship \_\_\_\_\_

Post Office Address \_\_\_\_\_

Full name sixth joint, inventor, if any \_\_\_\_\_

Inventor's Signature \_\_\_\_\_ Date \_\_\_\_\_

Residence \_\_\_\_\_ Citizenship \_\_\_\_\_

Post Office Address \_\_\_\_\_

Full name of seventh joint inventor, if any \_\_\_\_\_

Inventor's Signature \_\_\_\_\_ Date \_\_\_\_\_

Residence \_\_\_\_\_ Citizenship \_\_\_\_\_

Post Office Address \_\_\_\_\_

Full name eighth joint, inventor, if any \_\_\_\_\_

Inventor's Signature \_\_\_\_\_ Date \_\_\_\_\_

Residence \_\_\_\_\_ Citizenship \_\_\_\_\_

Post Office Address \_\_\_\_\_

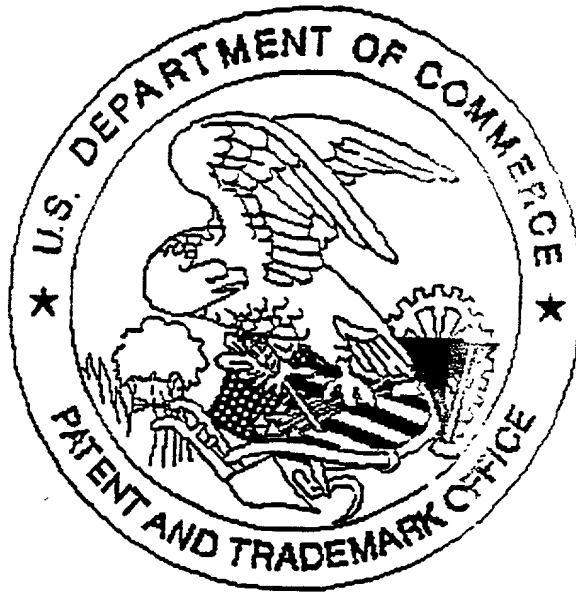
Full name ninth joint, inventor, if any \_\_\_\_\_

Inventor's Signature \_\_\_\_\_ Date \_\_\_\_\_

Residence \_\_\_\_\_ Citizenship \_\_\_\_\_

Post Office Address \_\_\_\_\_

United States Patent & Trademark Office  
Office of Initial Patent Examination -- Scanning Division



Application deficiencies were found during scanning:

☐ Page(s) 1 of Declaration were not present  
for scanning. (Document title)

☐ Page(s) \_\_\_\_\_ of \_\_\_\_\_ were not present  
for scanning. (Document title)

☐ Scanned copy is best available.

04449798-101898  
658101-86267450